

A VEHICLE INCLUDING A THREE-PHASE GENERATOR

RELATED APPLICATIONS

This application claims the benefit of prior filed co-pending U.S. Patent
5 Application No. 09/835,889, entitled A SMALL ENGINE VEHICLE INCLUDING A
GENERATOR, filed on April 16, 2001.

BACKGROUND OF THE INVENTION

The invention relates to a vehicle including a generator and, particularly, to a
vehicle including a generator having a plurality of wires disposed on a stator core in a
10 three-phase winding arrangement.

Small mobile generators are capable of providing a stable 120-volts root-mean-
square (VRMS), 60 hertz (Hz) power source. In addition, because the generators are
mobile, the generators may be transported to the desired location where electrical power is
needed. However, mobile generators are usually placed on a trailer and pulled to the
15 desired location by a vehicle.

Small-engine vehicles, such as riding lawn mowers, tractors, all-terrain vehicles
(ATV's), golf carts, etc., are robust vehicles capable of travelling to remote locations.
Small-engine vehicles are also able to pull small mobile generators. However, when the
desired location for the generator is in a remote location or across a treacherous landscape,
20 it may be difficult for the small-engine vehicle to pull the trailer carrying the generator to
the desired location.

When an operator owns a small-engine vehicle and a mobile generator, the
operator's costs increase. In addition, the operator is required to maintain two pieces of
machinery (e.g., maintain two engines). This may not be practical when the mobile
25 generator is infrequently used.

SUMMARY OF THE INVENTION

The invention provides a vehicle including a plurality of wheels, an internal
combustion engine having a drive shaft interconnected to drive at least one of the wheels,

a stator having a core, a plurality of wires disposed on the core in a three-phase winding arrangement, and a flywheel-rotor apparatus. The flywheel-rotor apparatus surrounds at least a portion of the stator and has an aperture that receives the drive shaft. The flywheel-rotor apparatus is operable to magnetically interact with the stator to produce a three-phase alternating current in the wires, and provides inertia to the internal combustion engine. The vehicle further includes power circuitry electrically connected to the wires. The power circuitry receives the three-phase alternating current and controllably generates a single-phase alternating current.

The stator, the plurality of wires, the flywheel-rotor apparatus, and the power circuitry form a generator. The vehicle of the present invention utilizes a three-phase winding arrangement because the power rating for a three-phase generator is typically greater than the power rating for a single-phase stator generator having the same weight. Other features, advantages and embodiments of the invention are set forth in the following detailed description, drawings and claims.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic diagram of a vehicle embodying the invention.

Fig. 2 is a partial side view of an engine and generator combination embodying the invention.

Fig. 3 is a partial perspective view of a stator and engine housing shown in Fig. 2.

Fig. 4 is a front plan view of a first stator.

Fig. 5 is a rear plan view of the first stator.

Fig. 6 is a rear plan view of a second stator.

Fig. 7 is a rear plan view of a third stator.

Fig. 8 is a rear plan view of a fourth stator.

Fig. 8A is a cross-sectional side view of the stator taken along line 8A-8A in Fig. 8.

Fig. 9 is a schematic representation of a stator-winding scheme.

Fig. 10 is a rear plan view of a flywheel-rotor apparatus.

Fig. 11 is a cross-sectional side view of the flywheel-rotor apparatus taken along line 11-11 in Fig. 10.

Fig. 12 is a schematic diagram of power circuitry schematically shown in Fig. 1.

Fig. 13 is an electrical schematic of a regulator schematically shown in Fig. 12.

5 Fig. 14 is an electrical schematic of a bridge circuit schematically shown in Fig. 12.

Fig. 15 is an electrical schematic of a first driver circuit schematically shown in Fig. 12.

Fig. 16 is an electrical schematic of a second driver circuit schematically shown in Fig. 12.

10 Fig. 17 is an electrical schematic of a current limit circuit schematically shown in Fig. 12.

Fig. 18 is an electrical schematic of a microprocessor, a voltage feedback circuit, a thermal shutdown circuit, and a voltage regulator schematically shown in Fig. 12.

Fig. 19 is a flow chart of a software program.

15 Figs. 20(a) and 20(b) are flowcharts of an interrupt service step shown in Fig. 19.

Fig. 21 is a first electrical schematic of a generator having a three-phase winding arrangement.

Fig. 22 is a second electrical schematic of a generator having a three-phase winding arrangement.

20 Fig. 23 is a third electrical schematic of a generator having a three-phase winding arrangement.

Fig. 24 is a fourth electrical schematic of a generator having a three-phase winding arrangement.

25 Fig. 25 is a fifth electrical schematic of a generator having a three-phase winding arrangement.

Before any embodiments of the invention are explained in full detail, it is to be understood that the invention is not limited in its application to the details of construction and the arrangement of components set forth in the following description or illustrated in the following drawings. The invention is capable of other embodiments and of being practiced or of being carried out in various ways. Also, it is to be understood that the phraseology and terminology used herein is for the purpose of description and should not be regarded as limiting. The use of "having," "including" and "comprising" and variations thereof herein is meant to encompass the items listed thereafter and equivalents thereof as well as additional items.

10 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

A vehicle 100 embodying the invention is schematically shown in Fig. 1. The vehicle 100 includes a plurality of wheels 105 and an internal combustion engine 110 (hereinafter referred to as "engine") interconnected to drive at least one of the wheels 105. That is, the engine 110 (also shown in Fig. 2) produces mechanical power causing a shaft 115 to rotate. One or more wheels 105 are interconnected with the rotating shaft 115 causing the interconnected wheels 105 to rotate. For the embodiment described herein, the vehicle 100 is a riding lawnmower with a Briggs & Stratton, Inc. INTEK™ or QUANTUM™ engine. However, the vehicle 100 may be any vehicle including an engine (e.g., a tractor, a lawnmower, an ATV, a golf cart, a motorcycle, etc.)

The vehicle 100 further includes an alternator or generator 120 interconnected with the engine 110. In general, the generator 120 includes a flywheel-rotor apparatus 125 (Fig. 2), a stator (e.g., stator 130, Fig. 2), power circuitry 135 (Fig. 1) and an electrical outlet 140 (Fig. 1). As best shown in Fig. 2 and shown in partial perspective view Fig. 3, the engine includes a housing 145, and the stator (e.g., stator 130) is interconnected (e.g., mounted) to the housing 145 by one or more fasteners (discussed below). Multiple embodiments of the stator 130 are shown in Figs. 3-8. As will become apparent below, other stators are possible.

With reference to Figs. 3, 4 and 5, the stator 130 includes a magnetically permeable stator core 150, which is of generally cylindrical shape. The core 150 is preferably formed by a plurality of stacked laminations 155 (best shown in Fig. 3) mechanically

interconnected together by one or more fasteners 160. Alternatively, in other embodiments, the core 150 is a solid core formed by one magnetically permeable member, or is magnetic powdered material compressed to form the core 150. The one or more fasteners 160 may include rivets, bolts, latches, etc., or even an epoxy or glue. In the
5 embodiment shown, the core 150 includes a first plurality of laminations 165 (best shown in Figs. 3 and 5) and a second plurality of laminations 170 (best shown in Figs. 3 and 5) fastened by four rivets 160 (best shown in Fig. 3).

The stator 130 includes a central opening 175 having a longitudinal axis 180 (best shown in Figs. 4 and 5). The stator 130 is mounted on the engine housing 145 such that
10 the central opening 175 receives at least a portion of the shaft 115. The stator 130 is secured to the housing 145 by one or more fasteners (e.g., rivet, bolt, latch, epoxy, glue, etc.) 185.

The stator core 150 forms at least one inner surface at least partially surrounding the longitudinal axis 180. For the embodiment shown and with reference to Fig. 5, the
15 first plurality of laminations 165 form a first inner surface 190 surrounding the longitudinal axis 180, and the second plurality of laminations 170 form a second inner surface 195 that extends in the circumferential direction with respect to the longitudinal axis 180. The second inner surface 195 is adjacent to the first inner surface 190 in the axial direction. The first plurality of laminations 165 further includes first, second, third
20 and fourth shelves 215, 220, 225 and 230, and first, second, third and fourth apertures 235, 240, 245 and 250. The first shelf 215 and a portion of the second inner surface 195 partially define a first recess 255, the second shelf 220 and a portion of the second inner surface 195 partially define a second recess 260, the third shelf 225 and a portion of the
25 second inner surface 195 partially define a third recess 265, and the fourth shelf 230 and a portion of the second inner surface 195 partially define a fourth recess 270.

The recesses 255, 260, 265 and 270 result in a volume of the stator core 150 that is "removed" as compared to a core that has only one plurality of substantially similarly designed laminations of cylindrical shape (discussed further below). The creation of the recesses 255, 260, 265 and 270 allows the recesses 255, 260, 265 and 270 to extend in the
30 circumferential direction for receiving a portion of the housing 145. By creating the

recesses 255, 260, 265 and 270, the stator 130 may be retrofitted on existing engines 110 where space is an issue.

For example, the housing 145 of a prior art engine may include a structure that would otherwise result in interference (e.g., rib structures 275 as shown in Fig. 3). In addition, the amount of engine compartment volume of the vehicle (i.e., the space "under the hood") may be of concern. In order to mount the generator 120 within the existing volume, the recesses 255, 260, 265 and 270 may be created in the stator 130. The recesses 255, 260, 265 and 270 allow one or more structures to extend into the one or more recesses 255, 260, 265 and 270 (e.g., the rib structures 275 shown in Fig. 3 extend into the one or more recesses 255, 260, 265 and 270.) This allows the stator 130 to sit closer to the engine 110 than if no recess was created.

Furthermore, one or more apertures 235, 240, 245 or 250 may extend through recesses 255, 260, 265 and 270, respectively, in the longitudinal direction. The apertures allow the stator 130 to be mounted closer to the engine housing 145. Having the stator 130 sit closer to the engine housing 145 allows for the engine and generator combination to be more compact and fit within an existing engine compartment volume of an existing vehicle.

In another embodiment, the stator core 276 (shown in Fig. 6) does not include one or more recesses. For this embodiment, space is not an issue. Rather, the stator 130 of this embodiment uses a "cylindrical" stator core 276 that generates more power than a core having at least one recess (e.g., a core 150 shown in Fig. 5).

In another embodiment, the second plurality of laminations partially defines one recess 277 that completely surrounds the longitudinal axis (shown in Fig. 7). In addition, for other embodiments, the number of recesses may vary and the amount of volume of a recess may vary.

In another embodiment, the recess 278 (shown in Fig. 8) is formed by at least three sets of laminations 279A, 279B and 279C. Specifically, the recess 278 is formed by gradually varying the radius R1, R2 and R3 of at least a portion of each set of laminations in the axial direction. For another embodiment, the one or more recesses may be defined

by a solid core. For some solid core embodiments, the one or more recesses are defined by a continuously varying radius in the longitudinal direction.

As best shown in Fig. 3, the stator 130 further includes a plurality of radially-extending teeth 280 and insulators 295 and 300 disposed on the teeth 280. The teeth 280 receive one or more electrical wires 305 that surround the insulators 295 and 300. The insulators 295 and 300 electrically isolate the wires 305 from the stator core 150. For the embodiment shown, the insulators 295 and 300 are first and second plastic insulators disposed on the core 150. Furthermore, for the embodiment's shown in Figs. 2-9, the number of teeth, which may be represented by the number (x), is equal to eighteen and the number of wires 305 is equal to two. However, the number of teeth may vary and the number of wires may vary. For example, in another embodiment, the number of teeth is equal to twenty. Increasing the number of teeth enables more power to be generated.

As best shown in Fig. 5, the teeth 280 (Fig. 3) are numbered from 1 to (x) (e.g., 1 to 18). As schematically shown in Fig. 9, a first wire 310 is wound around a first plurality of teeth to form a first plurality of coils 315. The first plurality of coils 315 create a first plurality of magnetic poles that interact with a plurality of magnets (discussed below) of the flywheel-rotor apparatus 125. A second wire 320 is wound around a second plurality of teeth to form a second plurality of coils 325. The second plurality of coils 325 create a second plurality of magnetic poles that interact with the plurality of magnets (discussed below) of the flywheel-rotor apparatus 125.

Specifically, for the embodiment schematically shown in Fig. 9, the core 150 includes a plurality of teeth numbered from 1 to 18. The first wire 310 is wound on the core 150 to form a first group of coils 315. The first group of coils 315 forms sixteen poles numbered 1 to 16 with each pole being formed on a respective tooth 1 to 16. The first wire 310 includes first and second ends 330 and 335 that exit the core between two adjacent teeth receiving the first group of coils 315. For the embodiment shown, the first and second ends 330 and 335 exit the core between the first and second teeth. The second wire 320 is disposed on the core 150 to form a second group of coils 325. The second group of coils 325 forms two poles numbered 17 and 18 with each pole being formed on a respective tooth 17 and 18. The second wire 320 includes third and fourth ends 340 and

345 that exit the core between two adjacent teeth receiving the second group of coils 325. For the embodiment shown, the third and fourth ends 340 and 345 exit the core between the seventeenth and eighteenth teeth.

Although the first group of coils 315 form a first group of poles 1 to 16 and the second group of coils 325 form a second group of poles 17 and 18, the number of poles of each group may vary. For example, the first group of poles may be numbered from one to $(x - n)$ where (x) is the total number of poles or teeth and (n) is the number of poles in the second group. For the second group, the poles are numbered from $(x - n + 1)$ to (x) . Thus, for the embodiment shown, (x) is eighteen and (n) is two. In another embodiment, (x) is twenty and (n) is two.

As will be discussed in further detail below, the flywheel-rotor apparatus 125 magnetically interacts with the stator 130 to generate a first voltage in the first wire 310 and generates a second voltage in the second wire 320, where the first voltage is greater than the second voltage. For example, the first voltage may be greater than approximately 200 V peak-to-peak, and the second voltage may be less than approximately 50 V peak-to-peak. The RMS voltage (and power) generated in each wire 310 or 320 is determined in part by the number of poles formed by the respective group of coils. In other words, varying the number of poles in a group of coils varies the voltage generated by the group of coils. For example, varying the number of poles for the first group of coils 315 from sixteen to eighteen increases the voltage generated by the first group of coils 315. Thus, depending on the voltage required by a group of coils, the number of poles (and teeth) may vary.

In addition, varying the number of turns of each coil also increases the RMS voltage generated by the group of coils. For example, if the number of turns for each coil changes from fifteen to twenty, then a higher voltage is generated for the group of coils.

For the winding scheme shown, the first and second ends 330 and 335 exit between two adjacent teeth receiving the first group of coils 315 (e.g., between teeth 1 and 2), and the third and fourth ends 340 and 345 exit between two adjacent teeth receiving the second group of coils 325 (e.g., between teeth 17 and 18). One reason for this is that undesirable noise is transmitted from the first and second ends to the third and fourth ends due to the

first group of coils generating a much higher voltage than the second group of coils. By having the first and second ends exit between two teeth of the first group of coils and by having the third and fourth ends exit between two teeth of the second group of coils, the noise is reduced. Although the embodiment described herein has the first and second ends exit between the first and second teeth, the first and second ends may exit between two other adjacent teeth receiving the first group of coils. Similarly, if the number of teeth receiving the second group of coils varies (e.g., (n) is equal to 4), then the third and fourth ends may exit between any two adjacent teeth receiving the second group of coils. However, if noise is not a concern, then other winding schemes may be used for the vehicle.

As shown in Fig. 9, the coils forming the odd numbered poles of the first group (e.g., poles 1, 3, 5, 7, 9, 11, 13, 15) are wound in a first direction (e.g., counterclockwise when viewing the core 150 from the rear), and the coils forming the even numbered poles of the first group (e.g., poles 2, 4, 6, 8, 10, 12, 14, 16) are wound in a second direction (e.g., counterclockwise when viewing the core 150 from the rear). The second direction is different than the first direction. Similarly, the coils forming the odd numbered poles of the second group (e.g., pole 17) are wound in the first direction, and the coils forming the even numbered poles of the second group (e.g., pole 18) are wound in the second direction.

One method of disposing the first and second wires 310 and 320 on the stator 130 is as follows. As schematically shown in Fig. 9, the first wire 310 is wound on the core 150 to form the first group of coils 315. The first group of coils 315 is formed by placing the first end 310 between teeth 1 and 2 and winding the wire around tooth 1 in the first direction. Next, the wire 310 is then wound to tooth 2 and a second coil is wound around tooth 2 in the second direction. The wire 310 then proceeds to tooth 3 and is wound around tooth 3 in the first direction. Next, the wire proceeds to tooth 4 and is wound around tooth 4 in the second direction. The winding on the first group of coils 315 is wound similarly for the remaining teeth 6-16, where the odd number poles are wound in the first direction and the even number of poles are wound in the second direction.

After winding the first wire 310 around tooth 16, the second wire 320 is cut to form the second end 330. An insulator 350 (e.g., a "shrink-tube" insulator) (Fig. 3) is disposed around the second end 330 and the first wire 310 is interwound back to tooth 2. That is, the first wire 310 is wound for a half turn around tooth 16, proceeds to the tooth 15, and is wound a half turn around tooth 15 (Fig. 9). The first wire 310 is wound for half turns around the remaining teeth back to tooth 2 and exits between teeth 1 and 2. The insulator 350 protects the half-turn winding from short-circuiting with the coils of the respective teeth. For example, the half-turn winding around tooth 7 does not short circuit with the coil that forms pole 7. The first and second ends 330 and 335 exit between the teeth 1 and 2 receiving the first and second coils. To strain relieve the first and second ends 330 and 335, an epoxy 355 (Fig. 5) may be applied to ends 330 and 335.

Similar to the first wire 310, the second wire 320 having third and fourth ends 340 and 345 is disposed on the core 150 to form the second group of coils 325. The second group of coils is formed by placing the third end 340 between tooth 17 and winding the wire around tooth 17 in the first direction. Next, the second wire 320 is then wound to tooth 18 and a second coil is wound around tooth 18 in the second direction. After winding the second wire 320 around tooth 18, the second wire 320 is cut to form the fourth end 345. The third and fourth ends 340 and 345 then exit between teeth 17 and 18. To strain relieve the third and fourth ends 340 and 345, an epoxy 360 (Fig. 5) may be applied to ends 340 and 345.

For the embodiment shown in Figs. 4-9, (n) is equal to two. However, if (n) is greater than two, then the winding scheme for the second wire 320 may be similar to the winding scheme for the first wire 310.

Referring back to Fig. 2, the generator 120 further includes a flywheel-rotor apparatus 125 that is coaxially aligned with the stator 130. As best shown in Figs. 10 and 11, the flywheel-rotor apparatus 125 includes a first central opening 370 for receiving the drive shaft 115 (Fig. 2). When the drive shaft 115 rotates, the flywheel-rotor apparatus 125 also rotates. The rotating flywheel-rotor apparatus 125 induces a magnetic field within the stator 130 causing a current to be generated in each wire 310 and 320.

Referring again to Figs. 10 and 11, the flywheel-rotor apparatus 125 includes a third inner surface 375 that at least partially surrounds the stator 130. The flywheel-rotor apparatus 125 further includes a plurality of rotor magnets 380 (e.g., eighteen magnets) mounted by fasteners (e.g., an epoxy or glue) to the third inner surface 375. In the
5 embodiment show, the rotor magnets 380 are neodymium-iron-boron (NdFeB) magnets. The flywheel-rotor apparatus 125 further includes an ignition magnet 385 mounted in the exterior of the flywheel-rotor apparatus 125 for generating an ignition signal, gearing teeth 390 disposed in the exterior of the flywheel-rotor apparatus 125 for interconnecting the flywheel-rotor apparatus 125 to an engine starting motor, apertures 395 for receiving a fan
10 plate having fins for cooling the engine and generator, and one or more balancing holes 400 used for balancing the flywheel-rotor apparatus 125.

The flywheel-rotor apparatus 125 includes a flywheel portion 402 interconnected with a rotor portion 404. The rotor portion 404 includes the magnets 380 and a back-iron 405. The rotor portion 404 is external to the stator 130 and magnetically interacts with the
15 stator 130. The flywheel portion 402 is an additional mass formed integral with the rotor portion 404 and may include a portion of the rotor back-iron 405. The flywheel portion 404 evens out the rotation of the drive shaft 115 while the engine 110 is running. The additional mass of the flywheel portion 402 is necessary for the internal-combustion engine 110 to operate properly and the rotor portion 404 is necessary to produce the
20 magnetic field for the generator 120. By combining the flywheel and rotor portions 402 and 404 into one apparatus 125, the number of parts is reduced and the amount of space required for the engine/generator combination 110 and 120 is reduced.

Referring back to Figs. 1 and 2, the generator 120 includes the power circuitry 135. The power circuitry 135 includes a first power circuitry and a second power circuitry,
25 which may be interconnected. In general, the first power circuitry receives a current and generates a single-phase alternating current (e.g., a 120-VRMS, 60-Hz signal), and the second power circuitry receives a current and generates a direct current. Fig. 12 shows a schematic diagram for one embodiment of the first power circuitry 450, and Figs. 13-18 show the electrical schematic of the first power circuitry 450. As will become more
30 apparent below, other embodiments of the power circuitry 135 may be used with the generator 120.

With reference to Figs. 12 and 13, the first power circuitry 450 includes a regulator 500. The regulator 500 receives a high-voltage, alternating-current (AC) input, and rectifies and regulates the received alternating current to generate a low-voltage DC output and a high-voltage DC output. The high-voltage, AC input is received at terminals W3 and W9 from first and second ends 330 and 335. For the embodiment shown in Figs. 12 and 13, the low-voltage DC output is approximately 15 VDC and the high-voltage DC output is approximately 150 VDC. However, in other embodiments, the low-voltage and high-voltage DC output voltages varies. Even further, for some embodiments, the high-voltage DC signal varies depending on the load attached to the power circuitry 135.

The high-voltage AC input may be a single-phase AC input generated using the above-described stator and winding arrangement, may be a single-phase AC input generated using another stator and winding arrangement, or a three-phase AC input generated using a three-phase winding arrangement. Unless specified otherwise, the description below with reference to Figs. 12-18 is for a single-phase AC input produced using the above-described stator and winding arrangement.

With reference to Fig. 13, the rectifier/regulator 500 includes a bridge rectifier 505. The bridge rectifier includes diodes D5 and D14 forming the upper portion of the bridge rectifier 505, and silicon-controlled rectifiers SCR1 and SCR3 forming the lower portion of the bridge rectifier 505. Diodes D4 and D15 provide an input or control signal for controlling the bridge rectifier 505. First filter 510 (resistor R29 and capacitor C4) filters the control signal provided to silicon-controlled rectifier SCR1 and second filter 515 (resistor R19 and capacitor C29) filters the control signal provided to silicon-control rectifier SCR2. Filtering the control signals provided to the silicon-controlled rectifiers SCR1 and SCR2 prevents the silicon-controlled rectifiers SCR1 and SCR2 from being too sensitive. During operation of the bridge rectifier 505, the rectifier 505 receives the high-voltage AC input generated by the stator 130 via inputs W9 and W3, rectifies and regulates the AC input in response to the control signals being provided to the silicon-controlled rectifiers SCR1 and SCR3, and provides a high-voltage DC output. The high-voltage DC output is stored on capacitors C6 and C3, which act as a DC bus. For the embodiment described, the high-voltage DC output is preferably 150 VDC. But, depending on the load attached to the first power circuitry 450, the DC bus may fluctuate

between 100 VDC and 150 VDC. If the stator 130 is a three-phase stator, then the bridge rectifier includes input W4, diode D7, silicon-control rectifier SCR2, and third filter 520 (resistor R30 and capacitor C5).

5 The rectifier/regulator 500 further includes a voltage monitor 525 and a trigger circuit 530. The voltage monitor 525 includes opto-isolator U2, precision voltage reference U1, zener diode D9 and resistors R28, R31 and R32. The trigger circuit 530 includes zener diodes D1 and D2, metal-oxide semiconductor field-effect transistors (MOSFETs) Q1 and Q2, opto-isolator U8, diac Q11, capacitors C1 and C2, and resistors R2, R3, R4, R5, R6, R8, R9, R10 and R27. The voltage monitor 525 and the trigger
10 circuit 530 control the bridge rectifier 505 to provide a continuous bus voltage between, 130 VDC and 150 VDC. Specifically, the trigger circuit 530 acts as a phase control that activates the silicon-control rectifiers SCR1 and SCR3 depending on the amount of power required to be added to the DC bus. For example, if the voltage monitor 525 senses a voltage on the DC bus greater than 150 VDC, then the trigger circuit 530 triggers the
15 silicon-controlled rectifiers SCR1 and SCR3 later in the phase of the high-voltage AC input. This results in less energy being provided to the DC bus and, therefore, a lower voltage. Similarly, if the voltage monitor 525 senses a voltage on the DC bus less than 150 VDC, then the trigger circuit 530 causes the silicon-controlled rectifiers SCR1 and SCR3 to activate sooner in the phase of the high-voltage AC input. This results in more
20 energy being provided to the DC bus and, consequently, a higher voltage. The voltage monitor 525 and the trigger circuit 530 attempt to regulate the DC bus voltage to approximately 150 VDC. However, depending on the load attached to the first power circuitry 450, the DC bus voltage may range between 130 VDC and 150 VDC. Of course, other voltages may be used for the DC bus.

25 The rectifier/regulator 500 further includes a low-voltage DC power supply 535. The low-voltage DC power supply 535 includes zener diode D10, capacitor C7 and resistors R33 and R34. The low-voltage DC power supply 535 receives the high-voltage DC output and produces a low-voltage DC output. For example, the low-voltage DC signal may be 15 VDC. Of course, other low-voltage DC outputs may be used.

Referring back to Fig. 12, the first power circuitry 450 further includes a bridge circuit 540. For the embodiment shown (Fig. 14), the bridge circuit 540 is an H-bridge circuit. The bridge circuit 540 includes first branch 545 (MOSFETs Q9, Q10 and Q14, resistor bridge 42, and resistor R22), second branch 550 (MOSFETs Q7, Q8, and Q15, resistor bridge R20, and resistor R25), third branch 555 (MOSFETs Q5, Q6, and Q12, resistor bridge R21, and resistor R14), and fourth branch 560 (MOSFETs Q3, Q4, and Q13, resistor bridge R13, and resistor R18). The bridge circuit 540 receives the high-voltage DC bus, and produces a 120-VRMS, 60-Hz AC output at terminals W1 and W2 in response to a plurality of drive signals 1aOUT, 1bOUT, 2aOUT and 2bOUT. Of course, other output voltages and frequencies (e.g., a 100-VRMS, 50-Hz AC output) may be produced. In addition, other bridge circuits may be used. For example, the embodiment shown in Fig. 14 has three MOSFETs in each branch. For a different embodiment, the number of MOSFETs may vary (e.g., two MOSFETs) depending on the capacity of the MOSFETs and the maximum expected current generated by the bridge circuit 540.

The drive signals 1aOUT, 1bOUT, 2aOUT and 2bOUT, and floating ground signals 1aSOURCE and 2aSOURCE are provided to the bridge circuit 540 by driver circuits 565 and 570 (Figs. 12, 15 and 16). First driver circuit 565 (Fig. 15) includes driver U5, capacitors C14, C15, C16, C17, C18, resistors R44, R50 and R51, and diode D12. The first drive circuit 565 drives the first and second branches 545 and 550 (Fig. 14) with the signals 1aOUT, 1bOUT and 1aSOURCE in response to gate signals GATE1a and GATE1b (discussed below). The second drive circuit 570 includes driver U4, capacitors C9, C10, C11, C12, C13, resistors R41, R52 and R53, and diode D11. The second drive circuit 570 (Fig. 16) drives the third and fourth branches 555 and 560 with the signals 2aOUT, 2bOUT and 2aSOURCE in response to the signals GATE2a and GATE2b (discussed below).

During operation of the bridge circuit 540 and the first and second driver circuits 565 and 570, an output signal is generated at terminals W1 and W2 (Fig. 14). The output is a pulse-width-modulated (PWM) signal having a frequency of approximately sixty Hz and a voltage of approximately 120 VRMS. Specifically, the first and second drivers 565 and 570 drive the MOSFETs Q3, Q4, Q5, Q6, Q7, Q8, Q9, Q10, Q12, Q13, Q14 and Q15, to produce a PWM 120-VRMS, 60-Hz signal at W1, W2. Each cycle includes a square

5 wave that is PWM to produce the required RMS voltage. The width of each half cycle is widened or narrowed depending on the DC bus voltage. If the DC bus voltage is low, then the width of each half cycle is widened. Conversely, if the DC bus voltage is high, then the width of the half cycle is narrowed. Thus, based on the drive signals provided to the bridge circuit 540, the output of the bridge circuit 540 maintains a relatively constant 120-VRMS, 60-Hz signal at outputs W1 and W2.

10 The output signals 1aOUT, 1bOUT, 1aSOURCE, 2aOUT, 2bOUT, and 2aSOURCE result from gate signals GATE1a, GATE1b, GATE2a and GATE2b. The GATE signals GATE1a, GATE1b, GATE2a, and GATE2b are generated by a microprocessor (discussed below). The first and second drivers U4 and U5 translate the gate signals GATE1a, GATE1b, GATE2a and GATE2b to 15-VDC drive signals (i.e., 1aOUT, 1bOUT, 2aOUT and 2bOUT). The 15-VDC drive signals are necessary to drive the MOSFETs Q3, Q4, Q5, Q6, Q7, Q8, Q9, Q10, Q12, Q13, Q14 and Q15. The signals 1aSOURCE and 2aSOURCE provide a floating reference to the bridge circuit 540.

15 The bridge circuit 540 shown in Fig. 14 includes a shunt resistor R11. The shunt resistor R11 is a power shunt for measuring the output current of the bridge circuit 540. The shunt resistor R11 is used to determine if an overload current is present i.e., if an operator is applying too large of a load to the bridge circuit 540. If too large of a load is present, the microprocessor (discussed below) narrows the pulse width of the 120-VRMS, 60-Hz output so that it cannot deliver too large of a current through the bridge circuit 540. The current measurement signal SHUNT is provided to a current limit circuit 575 (shown in Fig. 17). The current limit circuit 575 includes operational amplifiers U3A, U3B, resistors R1, R35, R36, R37, R38, R39, and R40, and capacitors C8 and C26. The operational amplifiers U3A amplifies the signal SHUNT, and the operational amplifier 25 U3B acts as a comparator between a reference signal and the amplified SHUNT signal. The reference signal is formed by resistors R39 and R40. The reference signal is set such that the peak current created by the bridge circuit cannot exceed a maximum peak current (e.g., forty-five amps). The maximum peak current is the maximum safe current the MOSFETs Q3, Q4, Q5, Q6, Q7, Q8, Q9, Q10, Q12, Q13, Q14 and Q15 can handle 30 without burning out. The current limit signal iLIMIT is provided to the microprocessor (discussed below).

As shown in Figs. 12 and 18, the first power circuitry 450 includes microprocessor U7. The microprocessor U7 receives and executes a software program from memory. Based on the inputs provided to the microprocessor U7, the microprocessor controls the driver circuits 565 and 570 with gate signals GATE1a, GATE1b, GATE2a and GATE2b. Specifically, the software determines the pulse width of each half cycle generated by the bridge circuit 540 based on the inputs provided to the microprocessor U7. For example, one of the input signals is the current limit signal iLIMIT. If the signal iLIMIT signifies that the current to the load is excessive, the microprocessor U7 controllably reduces the width of the PWM output signal.

As shown in Figs. 12 and 18, the first power circuitry 450 further includes a voltage feedback circuit 580. The voltage feedback circuit 580 includes resistors R48 and R49 and capacitor C23. The voltage feedback circuit 580 reduces the voltage from the DC bus to a 0-VDC to 5-VDC signal. The feedback from the DC bus informs the microprocessor U7 what the DC voltage is on the high-voltage bus.

As shown in Figs. 12 and 18, the first power circuitry 450 further includes a thermal shut down circuit 585. The thermal shut down circuit 585 includes a thermistor R15, a capacitor C24 and a resistor R12. The thermistor R15 is mounted near the MOSFETs Q3, Q4, Q5, Q6, Q7, Q8, Q9, Q10, Q12, Q13, Q14 and Q15, and senses the temperature generated by the bridge circuit 540. If the bridge circuit 540 generates an excessive temperature, thermistor R15 conducts and generates a high-logic signal TRIP. The microprocessor U7 receives the high-logic signal TRIP and stops producing the 120-VRMS, 60-Hz output. An example temperature may be 90-100 degrees Celsius. The higher the temperature gets, the sooner the thermal shut down circuit 585 generates the high-logic signal TRIP.

As shown in Figs. 12 and 18, the first power circuitry 450 further includes an oscillator XT1 for providing an oscillating signal to the microprocessor U7 and a voltage regulator U9 for generating a 5-VDC VCC signal. The first power circuitry 450 further includes a deactivate circuit 590 including resistors R63 and R64, capacitors C25 and C27 and optoisolator U6. The deactivate circuit 590 receives a 12-VDC blade signal 12BLADE or a 12-VDC input signal from terminals W7 and W8. When no twelve-volt

signal is present, the microprocessor U7 prevents the 120-VRMS, 60-Hz signal from being generated. Alternatively, if the 12-VDC signal is present then the first power circuitry 450 may generate an output. For example, if the generator 110 is mounted on a lawnmower, then the 12-BLADE signal informs the microprocessor U7 whether the blade is running.

- 5 If the blade is rotating, the first power circuitry 450 does not produce an output.

As shown in Figs. 12 and 18, inputs W5 and W6 receive a signal from a power switch. The power switch is an on/off switch that the operator activates and deactivates for controlling the first power circuitry 450. In the embodiment described herein, the power switch has to be turned ON from the OFF position in order for the power circuitry 135 to generate any power. For example, if an operator turns the engine on while the power switch is already in the ON position, then the microprocessor U7 does not allow an output from the power circuitry 135. This prevents an accidental output from being generated. In order to enable the power circuitry 135, the switch must be moved to the OFF position and then returned to the ON position.

15 Having described multiple embodiments of a vehicle 100 including a generator 120, the operation of the vehicle 100 will be discussed below. In operation, when an operator starts the vehicle 100, the engine 110 causes the drive shaft 115 to rotate and, consequently, the flywheel/rotor apparatus 125 to rotate. The flywheel/rotor apparatus 125 uses its inertia to smooth-out the rotation of the drive shaft 115. This allows the engine to run evenly for driving the rotation of the wheels 105. In addition, the magnetic fields produced by the rotor magnets 380 interact with the stator resulting in a current being generated in the first and second wires 310 and 320. The current produced in the second wire 320 is provided to the second power circuitry for powering the engine ignition system and/or the engine battery, and the current produced in the first wire 310 is provided to the first power circuitry 450. The current that is provided to the first power circuitry 450 is first regulated to produce a high-voltage DC output and a low voltage-DC output. The high-voltage DC output is stored in a storage device (e.g., capacitors C3 and C6). The storage device acts as a DC bus voltage. The low-voltage DC signal is provided to, among other things, the VCC regulator for generating a five-volt VCC signal. The 5-VDC VCC signal is provided to the microprocessor U7.

When the microprocessor U7 receives the 5-VDC VCC signal, the microprocessor U7 loads a software program from memory into the microprocessor U7. As shown in Fig. 19 and at step 710, the software initializes the microprocessor U7 and sets one or more interrupts. The initializing of the software includes initializing a main timer and setting an error flag ERR to high. The error flag ERR remains high until the software validates everything is properly running. The interrupts include a periodic interrupt (e.g., a 260 microsecond interrupt), and an interrupt occurring on the rising edge of the current limit signal iLIMIT. Of course, other interrupts, timers, and error flags may be included.

At step 715, the software increases the main timer until an interrupt occurs. The interrupt may be the periodic interrupt or an interrupt due to the current limit signal iLIMIT. Once an interrupt occurs then the software proceeds to perform an interrupt service (step 720).

At step 720, the software performs the interrupt service. In general terms, the software determines the cause of the interrupt and performs necessary actions based on the cause. As shown in Figs. 20a and 20b, if the interrupt is due to a high current (step 725), then the current being conducted through the MOSFETs is too high. When this occurs, the software sets a LIMIT flag to high (step 730). Setting the LIMIT flag to high informs later software modules to limit the amount of time the MOSFETs are on. Limiting the amount of time the MOSFETs are on reduces the amount of power and, consequently, current being conducted through the MOSFETs.

If the interrupt was due to a periodic interrupt (step 725), then the software proceeds to step 735. At step 735, the software samples the iLIMIT signal to determine if the amount of current being transmitted by the MOSFETs is within the desired limit. If the current is within limit, then the software sets the LIMIT flag to low (step 740). If the current is not within limit, then the software proceeds to step 745.

At step 745, the software determines whether the interrupt was a periodic interrupt. If the interrupt was a periodic interrupt, then software proceeds to step 750. Otherwise, the software returns from the interrupt service.

At step 750, the software resets the main timer for counting the next interrupt. At step 760, the software calls a HOTSub subroutine. The HOTSub subroutine checks whether the signal produced by the thermal shut down circuit is high. If the signal is high, then the MOSFETs are generating too much heat signifying that too much power is being generated. If the temperature is too hot, then a HOT counter is increased. If the temperature is satisfactory, then the HOT counter is decreased. If the HOT counter reaches a maximum count (e.g., fifteen), then the OUTPUT flag is set to low and the ERR flag is set to high. Setting the OUTPUT flag to low prevents gating of the MOSFETs (discussed below) and the ERR flag informs the processor a possible error is occurring. In addition a display may be used to inform the operator that the generator is too hot. The HOT counter includes a counting range (e.g., between zero and fifteen). Thus, the HOT counter allows the power circuitry 135 to generate some heat. But if too much heat is being generated for too long of a period of time, then the microprocessor U7 prevents electricity from being generated.

At step 765, the software determines whether the OUTPUT flag is set to high. If the OUTPUT flag is set to high, then the software has the microprocessor U7 generate the gating signals GATE1a, GATE1b, GATE2a, and GATE2b for controlling the bridge circuit 540 (step 770). The gating signals control the first and second drivers U4 and U5, which drive the bridge circuit 540. The gating signals are set by the software depending on the results of the PWSub subroutine (discussed below). In general, the software controls the gating of the microprocessor U7 based on the sensed bus voltage. The microprocessor U7 determines the pulse width PWM of the 120-VRMS, 60-Hz signal. If the OUTPUT flag is low (step 765), then the microprocessor U7 does not generate gating signals and the generator does not generate the 120-VRMS, 60-Hz signal (step 775).

At step 778, the software calls a DCSub subroutine, a VPWSub subroutine and a VOUTSub subroutine. The DCSub subroutine calculates the value of the DC bus voltage sensed by the voltage feedback circuit 580. The VPWSub subroutine determines the average value that each MOSFET is on. Based on the average value, the pulse width may be calculated. The VOUTSub subroutine calculates the RMS voltage being generated by the power circuitry 135. The RMS voltage is calculated using the sensed DC bus voltage and the calculated pulse width. For example, the RMS voltage may be calculated using a

sum of squares calculation. If the RMS voltage is too high or too low, the software can adjust the gating signals. In addition, if the voltage is less than 90 VRMS for thirty continuous seconds, then the OUTPUT flag is set to low and the ERR flag is set to high. Similarly, if the voltage is less than 50 VRMS for two continuous seconds, then the
5 OUTPUT flag is set to low and the ERR flag is set to high.

At step 780, the software determines whether sixty-four interrupts have occurred. If sixty-four interrupts have occurred, then the software performs an ONOFFSub subroutine, a BLADESub subroutine, and a PWSub subroutine (step 785). These subroutines do not need to be performed every interrupt. Of course, sixty-four is an
10 arbitrary number and other counters may be used. If sixty-four interrupts have not occurred (step 780), then the software increases the interrupt counter (step 790) and returns from the interrupt service.

The ONOFFSub subroutine determines whether the on/off switch for generating the 120-VRMS, 60-Hz signal is on. If the on/off switch is off then it sets the ERR flag to
15 low. Thus, the user has to "reset" the generator 120. For example, when the engine 110 first starts combusting, the generator 120 does not initially start generating power and accidentally cause damage to an attached load. The operator must turn the generator off and then on before the system will start generating. In addition, the software determines whether an initial DC bus voltage is greater than 120 VDC. If the DC bus voltage is
20 greater than 120 VDC, then the software sets the OUTPUT flag to high. Thus, before the first power circuitry 450 generates an output, the DC bus voltage must be at least 120 VDC. Of course, other voltages may be used.

The BLADESub subroutine determines whether either the blade signal or the interrupt signal is set to high. If either are high, then the ERR flag is set to high and the
25 output flag is set to low. For example, if the generator is mounted on a lawnmower, then the operator cannot have the blade on and generate the 120-VRMS, 60-Hz signal at the same time. Similarly, for other vehicles, other interrupts may be used.

The PWSub subroutine uses the values calculated by the VOUTSub, VPWSub and DCSub subroutine to determine which gate signals should be active for driving the bridge

circuit. Once the calculation is performed, the software resets the periodic interrupt count (step 795) and returns from the interrupt to step 715 (Fig. 19).

While multiple embodiments of a small engine vehicle 100 including a generator 120 have been discussed above, additional embodiments are discussed below and with reference to Figs. 21-25. Figs. 21-25 electrically show a generator 1000 capable of being used with the vehicle 100. The generator 1000 includes a flywheel-rotor apparatus (e.g., apparatus 125), a stator, a power circuitry 1002, and an electrical outlet 140.

In the embodiments below, the stator includes a stator core that is substantially similar to the stator core 276 (Fig. 6). However, in other embodiments, the generator 1000 includes different stator cores. Wires 1005, 1010 and 1015 are disposed on the stator core 276 in a three-phase arrangement or connection. Unless specified otherwise, for the winding arrangements herein, the wires 1005, 1010, 1015 are wound (e.g., by machinery or hand) on the core in a wye arrangement. The wires 1005, 1010 and 1015 are wound such that ends 1020, 1025 and 1030 are electrically connected together (e.g., by soldering), and ends 1035, 1040 and 1045 exit the stator core 276. For simplicity, ends 1020-1045 are only numbered in Fig. 21.

For the embodiment shown in Fig. 21, the stator core also receives wire 1050, which is placed on the core 276 in a single-phase arrangement such that ends 1055 and 1060 exit the core 276. The wires 1005A, 1010A and 1015A generate a high-voltage, three-phase alternating current, and the wire 1050 generates a low-voltage, single-phase alternating current. In some embodiments, the high-voltage, three-phase alternating current is greater than approximately 200 V peak-to-peak, and the low-voltage, single-phase alternating current is less than approximately 50 V peak-to-peak. It should be understood that the terms "high-voltage" and "low-voltage" are used for simplifying the description. Other terms may be used (e.g., "first," "second," etc.).

In one embodiment, the wires 1005A, 1010A, 1015A and 1050 are wound on the teeth of the stator core 276 such that the wire 1050 are electrically isolated from wires 1005A, 1010A and 1015A. That is, similar to Fig. 9, if the teeth are numbered 1 to (x), the wires 1005A, 1010A and 1015A are wound onto the teeth numbered from 1 to (x - n), and

the wire 1050 is wound onto the teeth numbered $(x - n + 1)$ to (x) . By isolating the wire 1050 from wires 1005A, 1010A and 1015A, the wire 1050 receives less undesirable noise.

In another embodiment, the wires 1005A, 1010A, 1015A are wound onto each of the teeth, and the wire 1050 is wound onto one or more teeth. For example, the wires
5 1005A, 1010A, 1015A are first wound onto the teeth numbered from 1 to (x) in a three-phase arrangement, and the wire 1050 is then wound over the wires 1005A, 1010A, 1015A in a single-phase arrangement. As compared to the previous embodiment, disposing the three-phase connection onto all of the teeth results in greater power being generated in the three-phase arrangement.

10 Referring again to Fig. 21, the generator 1000 includes power circuitry 1002. For the embodiment shown in Fig. 21, the power circuitry includes a first power circuitry 1065 that is substantially similar to the circuitry shown in Figs. 12-18. Specifically, the ends 1035, 1040 and 1045 are electrically connected to W3, W4 and W9 (Fig. 13). For other
15 embodiments, other circuit arrangements may be used in place of the circuitry shown in Figs. 12-18. The first power circuitry 1065 receives the high-voltage, three-phase current and controllably generates a single-phase, alternating current having a voltage between 90 VRMS and 135 VRMS, and having a frequency of 50 or 60 Hz. In one preferred embodiment, the voltage is approximately 120 VRMS, and the frequency is approximately 60 Hz.

20 Referring again to Fig. 21, the power circuitry 1002 includes a second power circuitry 1070. Similar to the single-phase embodiment described above, the ends 1055 and 1060 are connected to the second power circuitry 1070 for controllably generating a direct current. The direct current is preferably less than 50 VDC and, in one preferred embodiment, the direct current is approximately 12 VDC. The direct current is provided
25 to the vehicle and may be used for charging a battery or for the engine-ignition system. For other embodiments, the direct current is provided to the operator as a DC power source.

In one embodiment, the second power circuitry 1070 includes a voltage regulator 1075. A suitable voltage regulator capable of being used with the invention is available
30 from Tympanium Corporation of Malden, Massachusetts. Of course, other elements may

be added to the second power circuitry 1070. Additionally, while the first and second power circuitries 1065 and 1070 are shown separately, the circuitries 1065 and 1070 may be interconnected as one circuit.

For the embodiments shown in Figs. 22 and 23, the power circuitry 1002 includes the first power circuitry 1065 and a second power circuitry 1080 or 1085. The first power circuitry 1065 is substantially similar to the circuitry shown in Figs. 12-18. The first power circuitry 1065 receives the high-voltage, three-phase current, and controllably generates a single-phase, alternating current having a voltage between 90 VRMS and 135 VRMS. The second power circuitry 1080 or 1085 includes at least two connections electrically connected to the wires 1005A, 1010A and 1015A. At least one of the connections is a tap off of one of the phases. As used herein, the term "tap" means a connection made at some intermediate point in a winding.

With specific reference to Fig. 22, the second power circuitry 1080 includes two connections 1085 and 1090 interconnected with wire 1005A. The connection 1085 is interconnected to the end of the wire 1005A, and the connection 1090 is a tap off of the wire 1005A. In other embodiments, both connections 1085 and 1090 are taps off of the wire 1005A, or the connections 1085 and 1090 are interconnected to one of the other wires 1010A or 1015A. Similar to Fig. 21 and in one embodiment, the second power circuitry 1080 includes a voltage regulator 1075. The regulator 1075 receives the single-phase alternating current and produces a direct current less than 50 VDC (e.g., 12 VDC).

With specific reference to Fig. 23, the second power circuitry 1085 includes three connections 1095, 1100 and 1105 interconnected with the wires 1005A, 1010A and 1015A. Each connection 1095, 1100 and 1105 is tapped off of one of the wires 1005A, 1010A and 1015A, respectively. The second power circuitry 1085 receives a second three-phase, alternating current, which has a voltage less than the first three-phase alternating current provided to the first power circuitry 1065, and generates a direct current having a voltage less than 50 VDC (e.g., approximately 12 VDC). The second power circuitry 1085 includes a three-phase bridge 1110 and a voltage regulator 1115. The three-phase bridge 1110 may be incorporated with the voltage regulator 1115. In some circumstances, the embodiment shown in Fig. 23 may be preferred over Fig. 22. For

example, the embodiment shown in Fig. 23 has symmetrical taps, allowing a machine to more readily wind the arrangement shown in Fig. 23.

For the embodiments shown in Figs. 24 and 25, the power circuitry 1002 includes a first power circuitry 1125 and a second power circuitry 1130 or 1135. The first power circuitry 1125 receives a three-phase alternating current and generates a single-phase alternating current. For the first power circuitry 1125, the three-phase alternating current is less than the single-phase alternating current and, in one embodiment, is less than 50 V peak-to-peak. The single-phase alternating current produced by the first power circuitry 1125 includes a voltage between 90 and 135 VRMS, or a voltage between 190 and 250 VRMS. Additionally, the single-phase alternating current includes a frequency of 50 or 60 Hz. The first power circuitry 1125 includes circuit elements that increase the incoming voltage and that allow for the higher voltage range (i.e., the 190-250 VRMS rating). This allows the vehicle 100 to provide emergency power to a distribution box for a house. In the embodiments shown, the first power circuitry 1125 includes a three-phase inverter 1140 such as a CHEROKEE™ TS-1000 brand inverter available from NoOutage.Com LLC of Owings, MD. Of course, other components or circuitry may be included in the first power circuitry 1125.

The second power circuitry 1130 or 1135 includes at least two connections interconnected to the plurality of wires 1005B, 1010B, and 1015B. For the embodiment shown in Fig. 24, the second power circuitry 1130 includes first and second connections 1145 and 1150 electrically connected at ends 1020 and 1025. The second power circuitry 1130 receives a single-phase alternating current and produces a direct current less than 50 VDC (e.g., 12 VDC). In the embodiment shown in Fig. 24, the second power circuitry 1130 includes a voltage regulator 1155. Of course, other components or circuitry may be included in the second power circuitry 1130. It is also envisioned that, in some embodiments, the second power circuitry 1130 is interconnected with the first power circuitry 1125.

With specific reference to Fig. 25, the second power circuitry 1135 includes first, second and third connections 1160, 1165, and 1170 connected at ends 1035, 1040, and 1045, respectively. The second power circuitry 1135 receives a three-phase alternating

current and produces a direct current less than 50 VDC (e.g., 12 VDC). In the embodiment shown in Fig. 25, the second power circuitry includes a three-phase bridge 1175 and a voltage regulator 1180. Of course, other components or circuitry may be included in the second power circuitry 1135. It is also envisioned that, in some
5 embodiments, the second power circuitry 1135 is interconnected with the first power circuitry 1125.

As can be seen from the above, the present invention provides a vehicle including a generator. Various features and advantages of the invention are set forth in the following claims.

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